

APPENDIX **F**

ALL OTHER DEVELOPMENT SAMPLE DESIGN CALCULATIONS

A portion of the information provided in this appendix is referenced to the Los Angeles County Department of Public Works' *Low Impact Development Standards Manual* (LACDPW, 2014).

A map of the 85th percentile 24-hour rainfall depth and predominate soil type can be found at: <http://dpw.lacounty.gov/wrd/hydrologygis/>.

County of Los Angeles Department of Public Works, Analysis of 85th percentile 24-hour Rainfall Depth Analysis within the County of Los Angeles (February 2004) (<http://ladpw.org/wrd/publications>).

County of Los Angeles Department of Public Works, HydroCalc may be downloaded at: http://dpw.lacounty.gov/wmd/dsp_LowImpactDevelopment.cfm.

Appendix F: Sample Design Calculations & Worksheets

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FLOW RATE AND VOLUME CALCULATION EXAMPLE

Volume must be calculated for each tributary area to size each BMP.

PROJECT NAME: Commercial Site (Intersection of Western Ave & Washington Blvd)

Provide proposed project characteristics

A _{Total}	<u>1.15 Acres</u>
Type of Development	<u>Commercial</u>
Flow Path Length	<u>200 ft</u>
Flow Path Slope	<u>.01 (1%)</u>
% of Project Impervious	<u>87 %</u>
Predominate Soil Type #	<u>13</u>
Design Storm *	<u>85th percentile</u>

***Projects are required to use the larger of the Stormwater Quality Design Storm.**

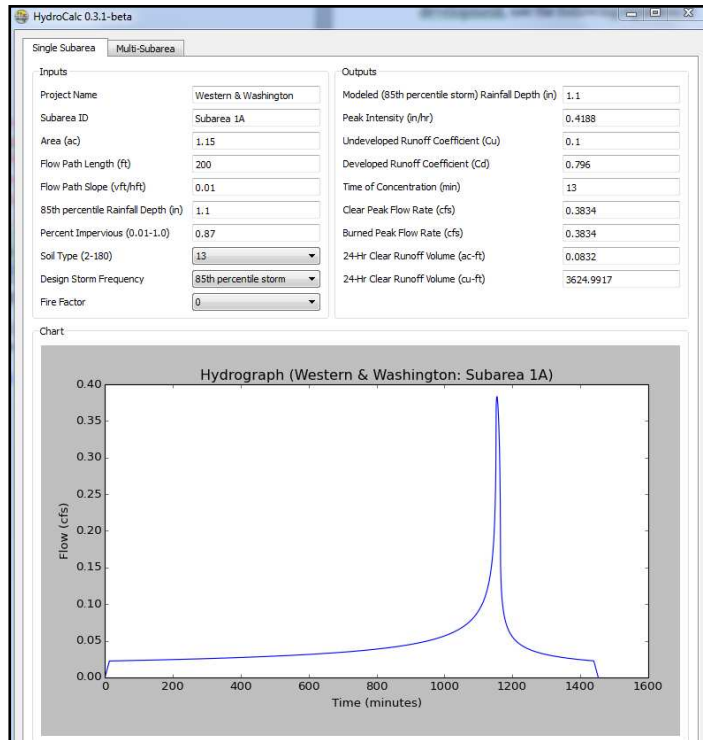
- The volume of runoff produced from a 0.75 inch (or 0.0625 ft) storm event, or
- The 85th percentile, 24-hr runoff event at this location = 1.1 inch (or 0.91 ft)

Refer to LA County Hydrology GIS Map
<http://dpw.lacounty.gov/wrd/hydrologygis/>

DETERMINING THE PEAK MITIGATED FLOW RATE (Q_{PM}):

Download [HydroCalc Calculator](#) (save onto your desktop). The HydroCalc Calculator allows the site designer/engineer to calculate runoff rates and volumes from the water quality storm.

http://dpw.lacounty.gov/wmd/dsp_LowImpactDevelopment.cfm



Appendix F: Sample Design Calculations & Worksheets

DETERMINING THE VOLUME (V_M)

In order to determine the volume (V_M) of stormwater runoff to be mitigated from the new development, use the larger storm volume from the following equation(s):

$$0.75 \text{ in Design Storm: } V_M (\text{ft}^3) = (0.625 \text{ Ft}) \cdot \text{Catchment Area (Sq. Ft)}$$

$$85^{\text{th}} \text{ Percentile Design Storm: } V_M (\text{ft}^3) = (\text{Storm Depth (Ft)}) \cdot \text{Catchment Area (Sq. Ft)}$$

Refer to LA County Hydrology GIS Map
<http://dpw.lacounty.gov/wrd/hydrologygis/>
and
http://ladpw.org/wrd/publication/engineering/Final_Report-Probability_Analysis_of_85th_Percentile_24-hr_Rainfall1.pdf

From Example, 1.1 inch > 0.75 inch, use
1.1 inch (0.91) Design Storm:

$A_I = 1.0$ acres

$A_P = 0.15$ acres

$$V_M (\text{ft}^3) = (0.091 \text{ ft}) \cdot \text{Catchment Area (in ft}^2)$$

$$\text{Catchment area (ft}^2) = (\text{impervious area} \cdot 0.9) + [(\text{pervious area} + \text{undeveloped area}) \cdot 0.1]$$

$$\text{Catchment area (ft}^2) = 43,560 \text{ ft}^2 \cdot [(1 \text{ ac} \cdot 0.9) + [(0.15 \text{ ac}) \cdot 0.1]] = 39,857.4 \text{ ft}^2$$

$$V_M (\text{ft}^3) = (0.091 \text{ ft}) \cdot 39,857.4 \text{ ft}^2$$

$$\underline{V_M = 3,627 \text{ ft}^3} \quad (\text{verify results with Hydrocalc results})$$

BMP TYPE AND SIZE

10. List the BMP Type(s) to be used in managing the calculated V_m , and size it per the design criteria listed in Section 4.

The following examples have been provided as a reference:

Infiltration BMPs:

- Infiltration Trench
- Dry Well
- Infiltration Basin

Capture and Use

- Rain Tanks
- Above / Below Grade Cisterns

Biofiltration

- Vegetated Swale
- Planter Box
- Biofiltration with underdrain

Infiltration BMP - Design for At Grade Infiltration Trench

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- $K_{\text{Sat, Measured}} = 2 \text{ in/hr}$ (Do not apply LA County reduction factor)
- $T = 48 \text{ hrs}$ (from Table 4.4)
- $FS = 3$ (from Table 4.4)
- Gravel void ratio = 40%

i. Determine $K_{\text{Sat, Design}}$

$$K_{\text{Sat, Design}} = \frac{K_{\text{Sat, Measured}}}{FS} = \frac{2 \text{ in/hr}}{3} = 0.667 \text{ in/hr}$$

ii. Determine Minimum Bottom Infiltration, A_{min} :

$$A_{\text{min}} = \frac{V_m \cdot 12 \text{ in/ft}}{K_{\text{Sat, Design}} \cdot T}$$

$$A_{\text{min}} = \frac{3,627 \text{ ft}^3 \cdot 12 \text{ in/ft}}{0.667 \text{ in/hr} \cdot 48 \text{ hr}} = 1,359 \text{ ft}^2$$

iii. Determine 3-hr infiltration volume, $V_{3\text{-hr}}$:

$$V_{3\text{-hr}} = A_{\text{min}} \cdot \left(\frac{K_{\text{Sat, Design}}}{12 \text{ in/ft}} \right) \cdot 3 \text{ hrs} = 1,359 \text{ ft}^2 \cdot \frac{0.667 \text{ in/hr}}{12 \text{ in/ft}} \cdot 3 \text{ hrs} = 226 \text{ ft}^3$$

iv. Determine the volume stored within the trench, $V_{\text{Trench Storage}}$:

$$V_{\text{Trench Storage}} = \frac{V_m}{\text{Void ratio}} = \frac{3,627 \text{ ft}^3}{0.4} = 9,067 \text{ ft}^3$$

v. Determine remaining volume of storage required:

$$V_{\text{Storage}} = V_{\text{Trench Storage}} - V_{3\text{-hr}} = 9,067 \text{ ft}^3 - 226 \text{ ft}^3 = 8,841 \text{ ft}^3$$

vi. Determine Design Depth:

$$D_{\text{Design}} = \frac{V_{\text{Storage}}}{A_{\text{min}}} = \frac{8,841 \text{ ft}^3}{1,359 \text{ ft}^2} = 6.5 \text{ ft}$$

Infiltration BMP – Design for Below Grade Dry Well

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- $K_{\text{Sat, Measured}} = 2 \text{ in/hr}$ (Do not apply LA County reduction factor)
- Gravel void ratio = 40%
- Factor of Safety = 3 (per table 4.4)
- $A_{\text{min}} = 934 \text{ ft}^2$
- $D = 6 \text{ ft}$ ($r = 3 \text{ ft}$)

i. Required dry well depth for the infiltration zone, h :

$$h = \frac{A_{\text{min}} - \pi r^2}{2\pi r}$$

$$h = \frac{934 \text{ ft}^2 - 28.26 \text{ ft}^2}{18.84 \text{ ft}} = 48 \text{ ft} *$$

* **Multiple dry wells may be used to achieve the equivalent infiltration zone.**

ii. Determine the dry well storage volume, V_{Storage} :
(assuming entirely filled with gravel)

$$V_{\text{Storage Dry Well}} = V_{\text{DryWell}} \bullet \text{Void Ratio}$$

$$= [\pi r^2 h] \bullet 0.4 = [\pi \bullet (3 \text{ ft})^2 \bullet 48 \text{ ft}] \bullet 0.4 = 543 \text{ ft}^3$$

iii. Determine 3-hr infiltration volume, $V_{3\text{-hr}}$:

$$V_{3\text{-hr}} = A_{\text{min}} \bullet \left(\frac{K_{\text{Sat, Design}}}{12 \text{ in/ft}} \right) \bullet 3 \text{ hrs} = 934 \text{ ft}^2 \bullet \frac{0.667 \text{ in/hr}}{12 \text{ in/ft}} \bullet 3 \text{ hrs} = 156 \text{ ft}^3$$

iv. Determine the additional required storage volume, $V_{\text{Additional Storage}}$:

$$V_{\text{Additional Storage}} = V_m - (V_{\text{Storage Dry Well}} + V_{3\text{-hr}}) = 3,627 \text{ ft}^3 - (543 \text{ ft}^3 + 156 \text{ ft}^3) = 2,928 \text{ ft}^3$$

2,928 ft³ of additional storage is required.

In order to satisfy the additional storage requirement, an upstream cistern or additional dry well chambers can be used. Some proprietary systems may provide additional storage capacity. Coordinate with manufactures.

Infiltration BMP – Design for Below Grade Infiltration Basin

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- $K_{\text{Sat, Measured}} = 2 \text{ in/hr}$ (Do not apply LA County reduction factor)
- $T = 96 \text{ hrs}$ (Table 4.4)

- i. Determine the design infiltration rate, $K_{\text{Sat, Design}}$:

$$K_{\text{Sat, Design}} = \frac{K_{\text{Sat, Measured}}}{FS} = \frac{2 \text{ in/hr}}{3} = 0.667 \text{ in/hr}$$

- ii. Determine Minimum Bottom Infiltration, A_{min} :

$$A_{\text{min}} = \frac{V_m \cdot 12 \text{ in/ft}}{K_{\text{sat, Design}} \cdot T}$$

$$A_{\text{min}} = \frac{3,627 \text{ ft}^3 \cdot 12 \text{ in/ft}}{0.667 \text{ in/hr} \cdot 96 \text{ hr}} = 680 \text{ ft}^2$$

- iii. Determine the Basin Design, D_{Basin} :

$$D_{\text{Basin}} = \frac{V_{\text{Storage}}}{A_{\text{min}}} = \frac{3,627 \text{ ft}^3}{680 \text{ ft}^2} = 5.3 \text{ ft}$$

Appendix F: Sample Design Calculations & Worksheets

Design for: Capture & Use

Givens:

- $V_{\text{Design}} = 3,627 \text{ ft}^3$ (from previous step)
- 0.15 acres of pervious area
- Medium Planting Type → Planting Factor = 0.4

- i. Determine the design volume in gallons:

$$V_{\text{Design}} (\text{gal}) = 3,627 \text{ ft}^3 \cdot 7.48 \frac{\text{gal}}{\text{ft}^3} = 27,130 \text{ gal}$$

- ii. Determine planting area (ft^2) within project limits:

$$\text{Planting Area} (\text{ft}^2) = 0.15 \text{ ac} \cdot 43,560 \frac{\text{ft}^2}{\text{ac}} = 6,534 \text{ ft}^2$$

- iii. Determine Planter Factor, PF, (ft^2):

(Planting factor may vary based on landscape design and plant types. Coordinate with Landscape Architect.)

$$\text{Planter Factor} (\text{ft}^2) = 0.4 \cdot 6,534 \text{ ft}^2 = 2,614 \text{ ft}^2$$

- iv. Determine the 7- month (Oct 1 – April 30) Estimated Total Water Use (ETWU):

$$ETWU_{(7\text{-month})} = ET_7 \cdot 0.62 \cdot PF$$

$$ETWU_{(7\text{-month})} = 21.7 \cdot 0.62 \cdot 2,614 \text{ ft}^2 = 35,163 \text{ gal}$$

- v. Verify $ETWU_{(7\text{-month})}$ is greater than or equal to the V_{Designed} :

$$ETWU_{(7\text{-month})} = 35,163 \text{ gal} \geq V_{\text{Design}} (\text{gal}) = 3,627 \text{ gal}$$

∴ CAPTURE & USE IS FEASIBLE

Biofiltration BMP – Design for Vegetated Swale*

Givens:

- base of swale = 5 ft
- Slope = 3%

i. Determine the swale base width and corresponding unit length:

- Per Table 4.6 → Select swale base of 5 ft with corresponding unit length of 470 ft/ac.

ii. Determine the total swale length:

$$L_{Swale(ft)} = 1.5 \cdot Catchment\ area\ (ft^2) \cdot \left(\frac{1\ acre}{43,560\ ft^2} \right) \cdot Swale\ length\ per\ catchment\ area\ (ft/acre)$$

$$Catchment\ area\ (ft^2) = (impervious\ area \cdot 0.9) + [(pervious\ area + undeveloped\ area) \cdot 0.1]$$

$$Catchment\ area\ (ft^2) = 43,560\ ft^2 \cdot [(1 \cdot 0.9) + [(0.15 + 0) \cdot 0.1]]$$

$$Catchment\ area\ (ft^2) = 39,857.4\ ft^2$$

$$L_{Swale(ft)} = 1.5 \cdot 39,857.4\ ft^2 \cdot \left(\frac{1\ acre}{43,560\ ft^2} \right) \cdot 470\ ft/acre$$

$$L_{Swale(ft)} = 645\ ft$$

iii. Determine the distance between check dams:

- Per Table 4.7 → At a 3% slope, the distance between check dams is 33 ft.

iv. Determine total number of check dams:

$$Total\ \#\ of\ dams = \frac{645}{33} = 19.5 \rightarrow \underline{use\ 20}$$

* Depending on the location of the swale, a geotechnical report may need to be submitted and approval from LADBS may be required.

Appendix F: Sample Design Calculations & Worksheets

Design for: Planter Box

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- Soil media infiltration rate, k_{sat} : 5 in/hr (Table 4.5)
- Time to fill 3 ft of media (24" soil, 12" gravel) to ponding depth, $T_{\text{Fill}} = 3 \text{ hrs}$ (Table 4.5) (per engineer, ex: 24" soil media, 12" gravel)
- Drawdown time, T (hr) = 48 hrs (Table 4.5)
- Ponding Depth = 1 ft (MAX) (Table 4.5)

i. Determine the design volume:

$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet V_m$$

$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet 3,627 \text{ ft}^3 = 5,440 \text{ ft}^3$$

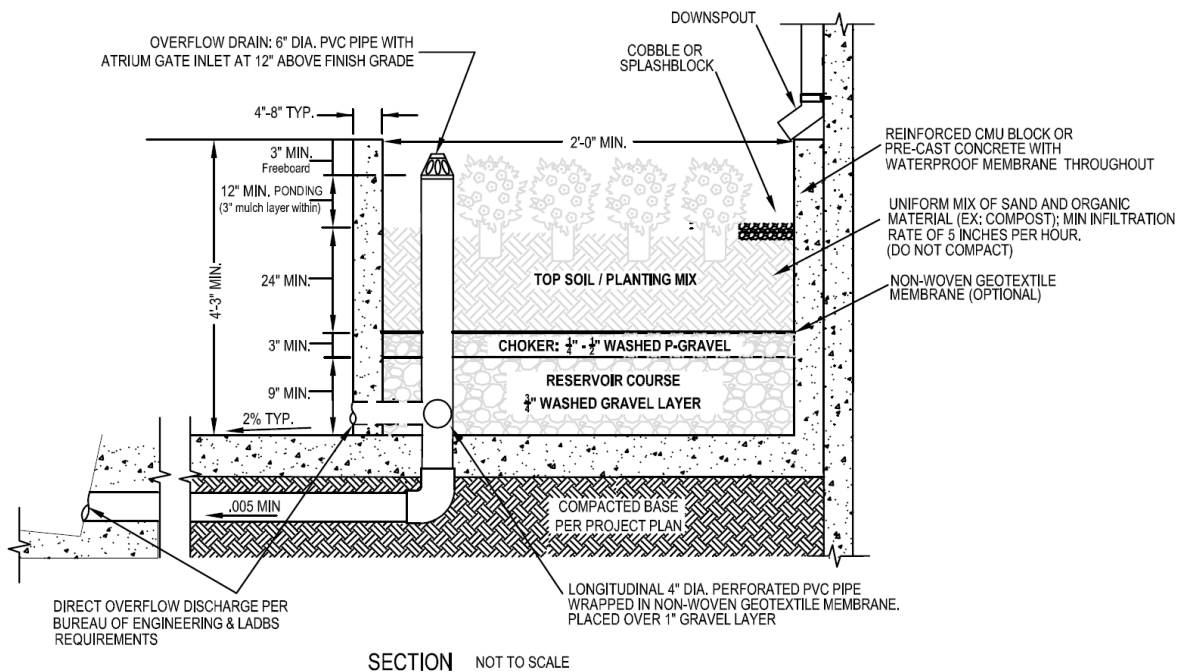
ii. Determine the design infiltration rate, $K_{\text{Sat,Design}}$:

$$K_{\text{Sat,Design}} = \frac{K_{\text{Sat,Media}}}{FS} = \frac{5 \text{ in/hr}}{2} = 2.5 \text{ in/hr}$$

iii. Calculate the BMP Surface Area, A_{min}^* :

$$A_{\text{min}} (\text{ft}^2) = \frac{V_{\text{Design}}}{\left[\left(\frac{T_{\text{Fill}} \bullet k_{\text{Sat,Design}}}{12 \text{ in/ft}} \right) + d_p \right]} = \frac{5,440 \text{ ft}^3}{\left[\left(\frac{3 \text{ hrs} \bullet 2.5 \text{ in/hr}}{12 \text{ in/hr}} \right) + 1 \text{ ft} \right]} = 3,347 \text{ ft}^2$$

*** Rule of thumb: With a max ponding depth of 1 ft, area needed is 5 - 6% of impervious area**



Appendix F: Sample Design Calculations & Worksheets

Alternative Design I

If ponding depth is reduced to 6" (0.50 ft), and the planting media is maintained at 24" and 12" of washed gravel, the minimum planter surface area would then be as follows:

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- Soil media infiltration rate, k_{sat} : 5 in/hr (Table 4.5)
- Time to fill 3 ft of media (24" soil, 12" gravel) to ponding depth, $T_{\text{Fill}} = 3 \text{ hrs}$ (Table 4.5) (per engineer, ex: 24" soil media, 12" gravel)
- Drawdown time, T (hr) = 48 hrs (Table 4.5)
- Ponding Depth, d_p (ft) = 6" = 0.50ft (Table 4.5)

i. Determine the design volume:

$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet V_m$$

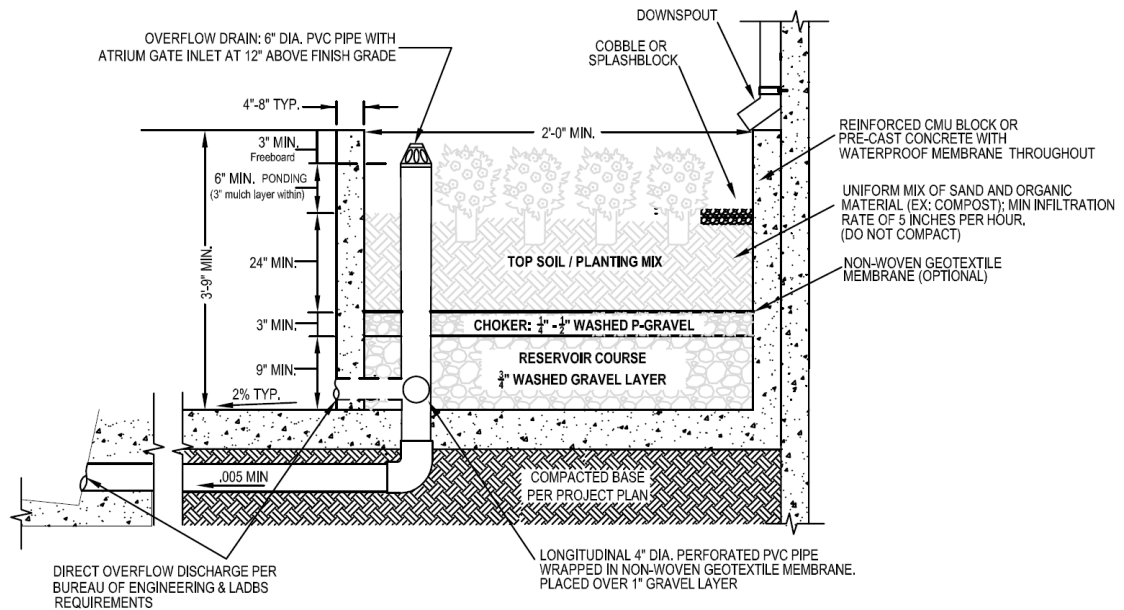
$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet 3,627 \text{ ft}^3 = 5,440 \text{ ft}^3$$

ii. Determine the design infiltration rate, $K_{\text{Sat,Design}}$:

$$K_{\text{Sat,Design}} = \frac{K_{\text{Sat,Media}}}{FS} = \frac{5 \text{ in/hr}}{2} = 2.5 \text{ in/hr}$$

iii. Calculate the BMP Surface Area, A_{min} :

$$A_{\text{min}} (\text{ft}^2) = \frac{V_{\text{Design}}}{\left[\frac{T_{\text{Fill}} \bullet k_{\text{Sat,Design}}}{12 \text{ in/ft}} + d_p \right]} = \frac{5,440 \text{ ft}^3}{\left[\frac{3 \text{ hr} \bullet 2.5 \text{ in/hr}}{12 \text{ in/ft}} + 0.50 \text{ ft} \right]} = 4,835 \text{ ft}^2$$



Appendix F: Sample Design Calculations & Worksheets

Alternative Design II

If ponding depth is reduced to 3" (0.25 ft) and planting media and gravel section total height are proposed to be 24" (2 ft), the minimum planter surface area would then be as follows:

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- Soil media infiltration rate, k_{sat} : 5 in/hr (Table 4.5)
- Time to fill 2 ft media (18" soil, 6" gravel) to ponding depth, $T_{\text{Fill}} = 2 \text{ hrs}$ (Table 4.5) (per engineer: 18" soil media, 6" gravel)
- Drawdown time, T (hr) = 48 hrs (Table 4.5)
- Ponding Depth, d_p (ft) = 3" (MIN) = 0.25 ft (Table 4.5)

i. Determine the design volume:

$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet V_m$$

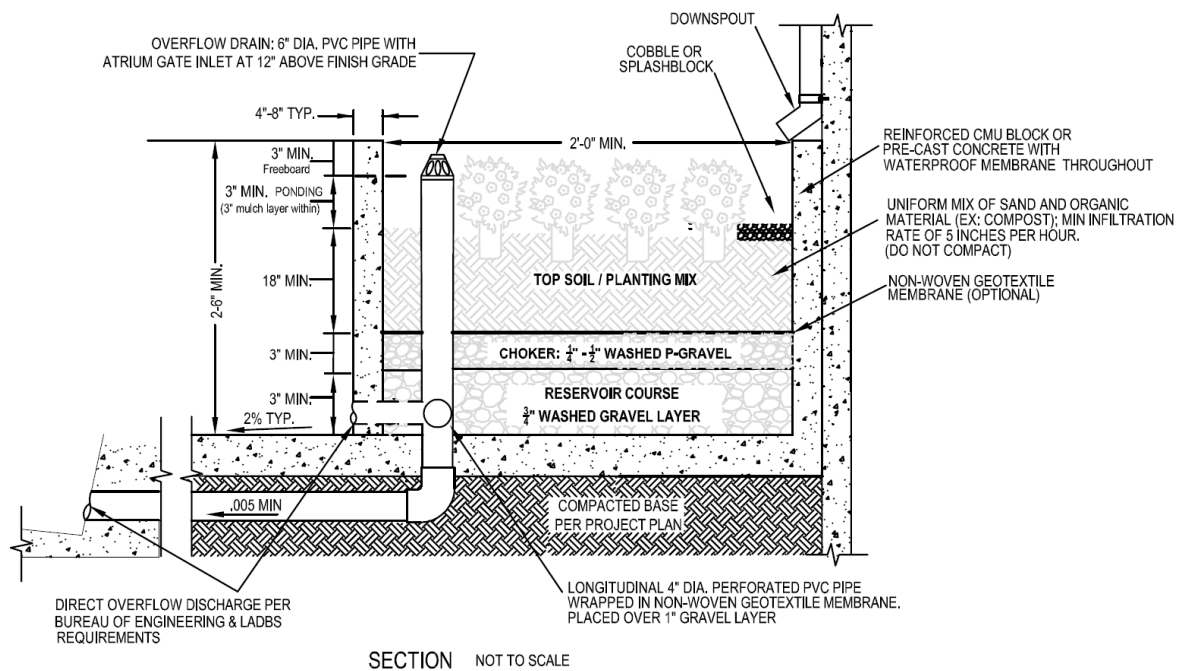
$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet 3,627 \text{ ft}^3 = 5,440 \text{ ft}^3$$

ii. Determine the design infiltration rate, $K_{\text{Sat,Design}}$:

$$K_{\text{Sat,Design}} = \frac{K_{\text{Sat,Media}}}{FS} = \frac{5 \text{ in/hr}}{2} = 2.5 \text{ in/hr}$$

iii. Calculate the BMP Surface Area, A_{min} :

$$A_{\text{min}} (\text{ft}^2) = \frac{V_{\text{Design}}}{\left[\left(\frac{T_{\text{Fill}} \bullet k_{\text{Sat,Design}}}{12 \text{ in/ft}} \right) + d_p \right]} = \frac{5,440 \text{ ft}^3}{\left[\left(\frac{2 \text{ hr} \bullet 2.5 \text{ in/hr}}{12 \text{ in/ft}} \right) + 0.25 \text{ ft} \right]} = 8,160 \text{ ft}^2$$



Design for: Biofiltration with underdrain (at grade)

Givens:

- $V_m = 3,627 \text{ ft}^3$ (from previous step)
- Soil media infiltration rate, k_{sat} : 5 in/hr (Table 4.5)
- Time to fill 3 ft of media (24" soil, 12" gravel) to ponding depth, $T_{\text{Fill}} = 3 \text{ hrs}$ (Table 4.5) (per engineer, ex: 24" soil media, 12" gravel)
- Drawdown time, T (hr) = 48 hrs (Table 4.5)
- Ponding Depth = 15 in. (per engineer, 18 in max) (Table 4.5)
- Side slopes = 3:1

iv. Determine the design volume:

$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet V_m$$

$$V_{\text{Design}} (\text{ft}^3) = 1.5 \bullet 3,627 \text{ ft}^3 = 5,440 \text{ ft}^3$$

v. Determine the design infiltration rate, $K_{\text{Sat,Design}}$:

$$K_{\text{Sat,Design}} = \frac{K_{\text{Sat,Media}}}{FS} = \frac{5 \text{ in/hr}}{2} = 2.5 \text{ in/hr}$$

vi. Calculate the BMP Surface Area, A_{min}^* :

$$A_{\text{min}} (\text{ft}^2) = \frac{V_{\text{Design}}}{\left[\left(\frac{T_{\text{Fill}} \bullet k_{\text{Sat,Design}}}{12 \text{ in/ft}} \right) + d_p \right]} = \frac{5,440 \text{ ft}^3}{\left[\left(\frac{3 \text{ hrs} \bullet 2.5 \text{ in/hr}}{12 \text{ in/hr}} \right) + 1.25 \text{ ft} \right]} = 2,901.3 \text{ ft}^2$$